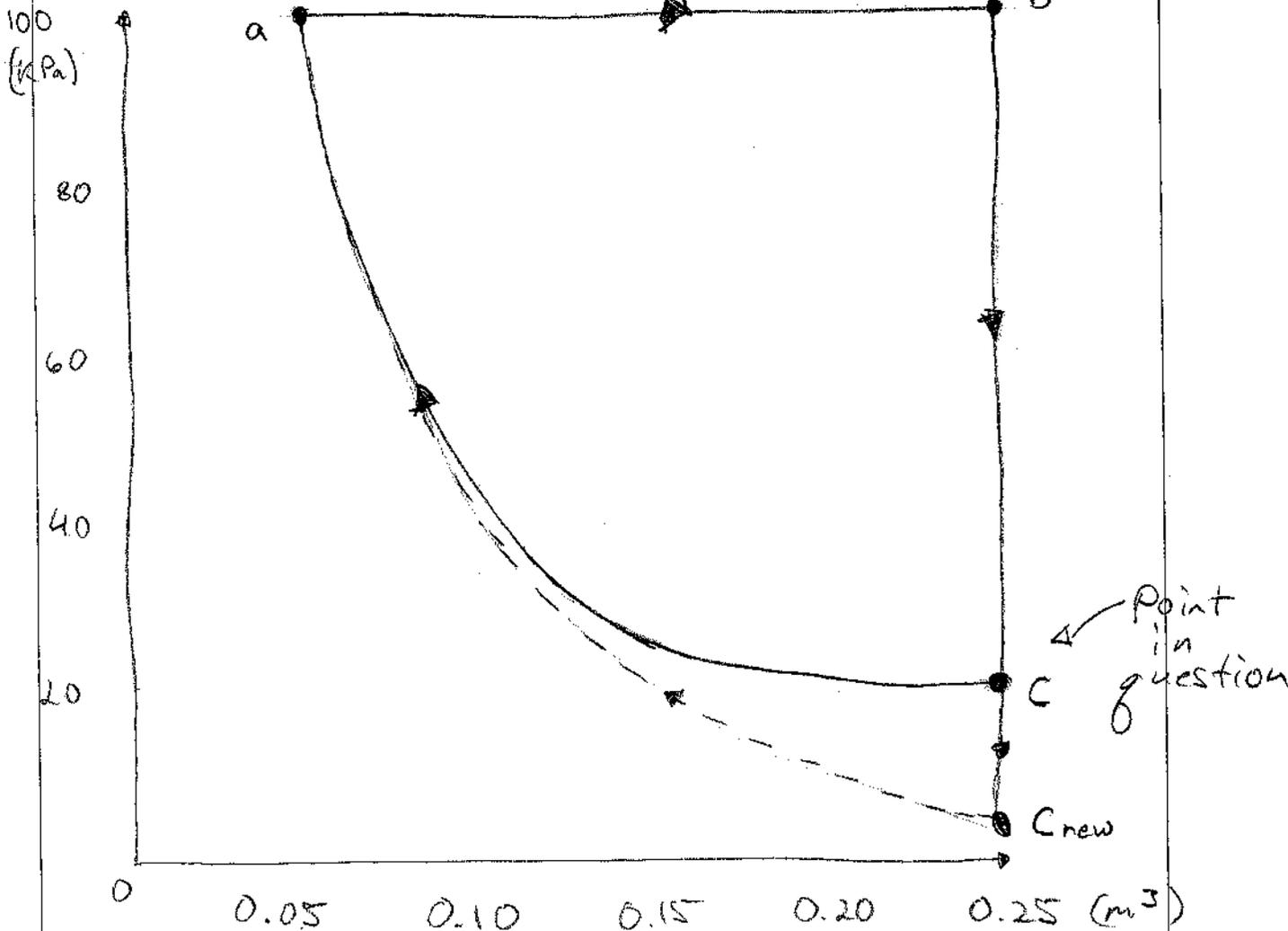


1) Draw a picture



a) check for adiabatic  $\gamma = 1.667$  for ideal gas

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$
$$P_2 = P_1 \left( \frac{V_1}{V_2} \right)^\gamma = 100 \text{ kPa} \left( \frac{0.05}{0.25} \right)^{1.667}$$
$$= 6.84 \text{ kPa} \quad \bullet$$

no! not possible

b) modify point c to go to 6.84 kPa

e) i) know total entropy in a cycle with reversible gas  $\Delta S_{\text{cycle}} = 0$

$$\Delta S_{12} = \int_1^2 \frac{dQ}{T} = C_V \ln\left(\frac{T_2}{T_1}\right) + Nk_B \ln\left(\frac{V_2}{V_1}\right)$$

For (a-b) have 
$$\Delta S_{ab} = C_V \ln\left(\frac{T_b}{T_a}\right) + Nk_B \ln\left(\frac{V_b}{V_a}\right)$$

$$= C_P \ln T_b/T_a$$

For (b-c) have

$$\Delta S_{bc} = C_V \ln T_c/T_b$$

$$= C_V \ln\left(\frac{T_a}{T_b} \cdot \left(\frac{V_a}{V_c}\right)^{\gamma-1}\right)$$

(use  $P_a V_a^\gamma = P_c V_c^\gamma$   
or  $T_a V_a^{\gamma-1} = T_c V_c^{\gamma-1}$ )

$$= C_V \ln\left(\frac{T_a}{T_b}\right) + C_V \left(\frac{C_P}{C_V} - 1\right) \ln\left(\frac{V_a}{V_c}\right)$$

$$= C_V \ln\left(\frac{T_a}{T_b}\right) + (C_P - C_V) \ln\left(\frac{V_a}{V_c}\right)$$

but  $V_c = V_b$  and  $C_P - C_V = Nk_B$

so 
$$\Delta S_{bc} = C_V \ln\left(\frac{T_a}{T_b}\right) + Nk_B \ln\left(\frac{V_a}{V_b}\right)$$

∴ since  $\Delta S_{ab} + \Delta S_{bc} = 0$   $\Delta S_{ca} = 0$  too

which we would have guessed since  $dQ = 0$

in an adiabatic process

ii) The efficiency of a cycle is defined

$\frac{\text{Work you get}}{\text{energy you pay for}}$

for a cycle  $\Delta E_{\text{INT}} = 0 = Q_{\text{put in}} - |Q|_{\text{take out}} - W_{\text{net}}$

in the isobaric process

$$Q_{\text{put in}} = C_P \Delta T$$

$$W_{\text{done by gas}} = p \Delta V$$

isochoric process  $|Q_{\text{take out}}| = C_V \Delta T$  (no work done)

adiabatic

$$\Delta E_{\text{INT}} = W_{\text{done by gas}}$$

c) hottest temp is at biggest  $PV = P_B V_B$

lowest temp is at lowest  $PV = P_C V_C$

$$\begin{aligned} \text{Maximum efficiency} &= 1 - \frac{T_C}{T_H} = 1 - \frac{P_C V_C}{P_B V_B} \quad \leftarrow Nk_B T_C \\ &= 1 - \frac{(6.84 \text{ kPa})(0.25 \text{ m}^3)}{(100 \text{ kPa})(0.25 \text{ m}^3)} \quad \leftarrow Nk_B T_B \\ &= 0.932 \quad \text{wow!} \end{aligned}$$

Our actual efficiency will be  $\frac{W}{Q_H} = 1 - \frac{|Q_C|}{Q_H}$

Since no heat flowed during the adiabatic cycle

$$Q_H = C_p \Delta T_{ab} = \frac{5}{2} (P_b V_b - P_a V_a)$$

$$Q_C = C_v \Delta T_{bc} = \frac{3}{2} (P_c V_c - P_b V_b)$$

$$\begin{aligned} \epsilon &= 1 - \frac{\frac{3}{2} |(6.84(0.25) - 100(0.25))|}{\frac{5}{2} ((100)(0.25) - 100(0.05))} \\ &= 1 - \frac{34.9 \text{ kJ}}{50.0 \text{ kJ}} = 0.30 \quad \text{yikes, better check} \end{aligned}$$

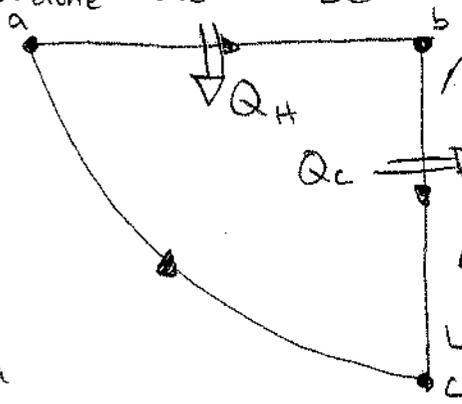
Work should be  $Q_H - |Q_C| = 15.1 \text{ kJ}$

$$\text{should be } W_{ab} + W_{ca} = P_a (V_b - V_a) + \int_{V_c}^{V_a} \frac{P_c V_c^\gamma}{V^\gamma} dV$$

$$\begin{aligned} &= P_a (V_b - V_a) - \frac{P_c V_c^\gamma}{(\gamma-1)} \left( \frac{1}{V_a^{\gamma-1}} - \frac{1}{V_c^{\gamma-1}} \right) \\ &= P_a (V_b - V_a) - \frac{1}{(\gamma-1)} \left[ \frac{P_c V_c^\gamma}{V_a^\gamma} V_a - P_c V_c \right] \\ &= P_a (V_b - V_a) - \left( \frac{1}{\gamma-1} \right) [P_a V_a - P_c V_c] \\ &= P_a (V_b - V_a) - \left( \frac{C_v}{C_p - C_v} \right) [P_a V_a - P_c V_c] \\ &= \frac{C_p (P_b V_b - P_a V_a) - C_v (P_b V_b - P_a V_a) - C_v (P_a V_a - P_c V_c)}{Nk_B} \\ &= \frac{5}{2} (P_b V_b - P_a V_a) - \frac{3}{2} (P_b V_b - P_c V_c) \quad \text{same} \end{aligned}$$

lets look at the whole cycle now

a-b  $\left\{ \begin{aligned} \Delta E_{int} &= \frac{3}{2} (100 \text{ kPa} [0.25 \text{ m}^3 - 0.05 \text{ m}^3]) = 30 \text{ kJ} \\ W_{done} &= 20 \text{ kJ} \quad \Delta Q = 50 \text{ kJ} \text{ (heat flowed into gas)} \end{aligned} \right.$



b-c  $\left\{ \begin{aligned} \Delta E_{int} &= \frac{3}{2} (6.84 \text{ kPa} (0.25 \text{ m}^3) - 100 \text{ kPa} (0.25 \text{ m}^3)) \\ &= -34.9 \text{ kJ} \\ \Delta Q &= -34.9 \text{ kJ} \\ W &= 0 \end{aligned} \right.$

c-D a  $\Delta E_{int} = \frac{3}{2} (100 \text{ kPa} (0.05 \text{ m}^3) - 6.84 \text{ kPa} (0.25 \text{ m}^3)) = 4.94 \text{ kJ}$

$\Delta Q = 0$   
 $W = -4.94 \text{ kJ}$

check  $\Delta E_{int} = 0$  for cycle

$\epsilon = \frac{20 \text{ kJ} - 4.94 \text{ kJ}}{50 \text{ kJ}} = 0.30$

check entropies

$\Delta S_{ab} = C_p \ln \left( \frac{P_b V_b}{P_a V_a} \right) = N k_B \frac{5}{2} \ln \left( \frac{(100 \text{ kPa})(0.25 \text{ m}^3)}{(100 \text{ kPa})(0.05 \text{ m}^3)} \right)$   
 $= (N k_B) 4.02$

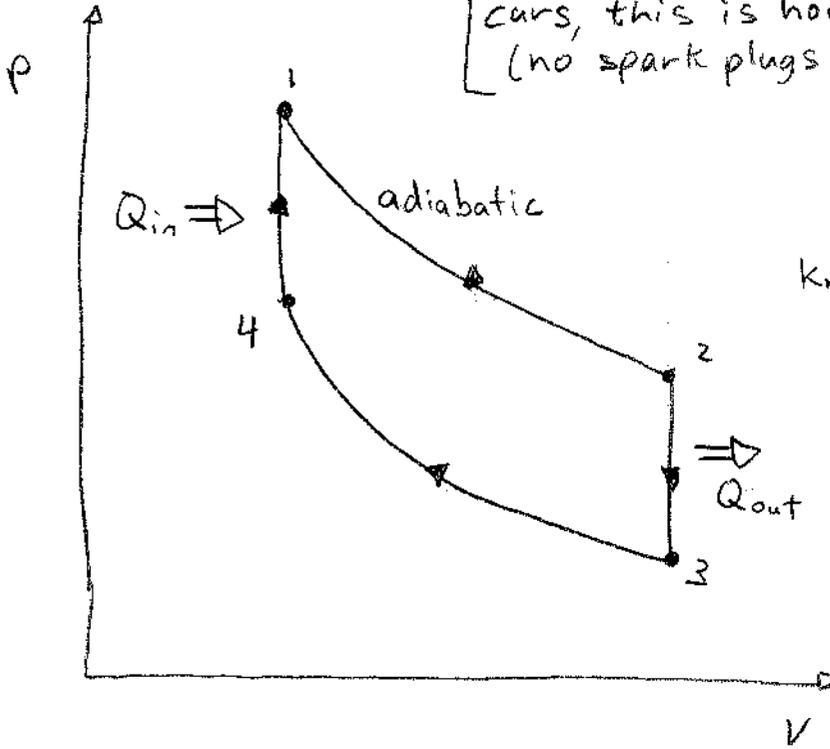
$\Delta S_{bc} = C_v \ln \left( \frac{P_c V_c}{P_b V_b} \right)$   
 $= N k_B \frac{3}{2} \ln \left( \frac{(6.84 \text{ kPa})(0.05 \text{ m}^3)}{(100 \text{ kPa})(0.05 \text{ m}^3)} \right) = (N k_B) (-4.02)$

$\Delta S_{ca} = 0$

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Otto Cycle

gas can spontaneously ignite if it is compressed too much. In diesel cars, this is how the fuel burns - (no spark plugs in a diesel engine!)  
 need to find; higher efficiency



efficiency in terms of temp & volume

know

$$\epsilon = 1 - \frac{|Q_c|}{Q_H} = \frac{W}{Q_H}$$

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$

$$P_3 V_3^\gamma = P_4 V_4^\gamma$$

$$\Delta Q_{12} = 0 = \Delta Q_{34}$$

$$W_{23} = 0 = W_{41}$$

$Q_H$  or  $Q$  we put in is only going to occur on the 4-1 transition

$$Q_H = C_v(T_1 - T_4)$$

$Q_c$  or  $Q$  we take out only occurs on the 2-3 transition

$$|Q_c| = C_v(T_2 - T_3)$$

$$\epsilon = 1 - \frac{C_v(T_2 - T_3)}{C_v(T_1 - T_4)} = 1 - \frac{(T_2 - T_3)}{(T_1 - T_4)}$$

$$= 1 - \frac{P_2 V_2 - P_3 V_3}{P_1 V_1 - P_4 V_4} = 1 - \frac{(P_2 - P_3) V_2}{(P_1 - P_4) V_1}$$

$$P_2 = P_1 \left(\frac{V_1}{V_2}\right)^\gamma, \quad P_3 = P_4 \left(\frac{V_4}{V_3}\right)^\gamma = P_4 \left(\frac{V_1}{V_2}\right)^\gamma$$

$$\epsilon = 1 - \frac{(P_1 \left(\frac{V_1}{V_2}\right)^\gamma - P_4 \left(\frac{V_1}{V_2}\right)^\gamma) V_2}{(P_1 - P_4) V_1} = 1 - \left(\frac{V_1}{V_2}\right)^{\gamma-1}$$